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Hirasugar Institute of Technology, Nidasoshi.

Inculcating Values, Promoting Prosperity

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E&E Engg. Dept.

Exam.

Internal Assessment

Odd Sem(2017-18)

THIRD INTERNAL ASSESSMENTSem: III
Date: 20-11-2017Sub: EMT
Time: 3.00PM – 4.00PMSub. Code: 15EC36
Max. Marks: 25*Note: Answer two full questions, draw sketches wherever necessary.*

Q. No	Discription of Question		Marks	CO
1	a	Wheteher the following potential fields satisfy the Laplace's equation or not? i) $V = [Ar^4 + Br^{-4}] \sin 4\Phi$ ii) $V = r \cos \Theta + \Phi$	6	CO206.3
	b	Derive an expression for magnetic field intensity H due to a long straight conductor.	6	CO206.3
OR				
2	a	Use Laplace's equation to find the capacitance per unit length of a co-axial cable of inner radius 'a' m and outer radius 'b' m. Assume $V=V_0$ at $r=a$ and $V=0$ at $r=b$.	6	CO206.3
	b	State and prove Stoke's theorem including the concept of curl.	6	CO206.4
3	a	A current element $I_1 \Delta L_1 = 10^{-5} a_z$ A.m is located at P1(1,0,0) while the other element $I_2 \Delta L_2 = 10^{-5} (0.6a_x - 2a_y + 3a_z)$ A.m is at P2 (-1,0,0) both in free space. Find the vector force exerted on $I_2 \Delta L_2$ by $I_1 \Delta L_1$.	6	CO206.7
	b	Explain the concept of displacement current with relevant equations.	7	CO206.5
OR				
4	a	Derive the boundary conditions at the interface of two magnetic materials	6	CO206.5
	b	Briefly explain Maxwell's equations.	7	CO206.5

P01-P03
P06-P08
P012

Course Coordinator


Module Coordinator


HOD



III - IA SCHEME OF EVALUATION

Sem : 3		Subject : EMT	Sub Code : ISEC36	Date : 20-11-17	
Q. No.	Bit	Description	Marks	Mapped CO's	
1	a.	<p> $\Rightarrow V = [Ar^4 + Br^4] \sin 4\phi$ Cylindrical system. $\nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial V}{\partial r} \right) + \frac{1}{r^2} \left(\frac{\partial^2 V}{\partial \phi^2} \right) + \frac{\partial^2 V}{\partial z^2}$ $\frac{1}{r} \frac{\partial}{\partial r} \left[r \frac{\partial V}{\partial r} \right] = \frac{\sin 4\phi}{r} [16Ar^3 + 16Br^5]$ $\frac{1}{r^2} \frac{\partial^2 V}{\partial \phi^2} = -\sin 4\phi [16Ar^2 + 16Br^6]$ $\frac{\partial^2 V}{\partial z^2} = 0$ $\nabla^2 V = \sin 4\phi [16Ar^2 + 16Br^6] - \sin 4\phi [16Ar^2 + 16Br^6] = 0$ </p>	1/2	CO206/4	
	b.	<p> $\Rightarrow V = r \cos \theta + \phi$ Spherical system. $\nabla^2 V = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial V}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial V}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2}$ $\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial V}{\partial r} \right) = r^2 \frac{\partial}{\partial r} [r \cos \theta + \phi] = r^2 \cos \theta$ $\frac{\sin \theta}{\partial \theta} \frac{\partial V}{\partial \theta} = \sin \theta \frac{\partial}{\partial \theta} [r \cos \theta + \phi] = -r^2 \sin \theta$ $\frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2} = \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2}{\partial \phi^2} [r \cos \theta + \phi] = 0$ $= \frac{2}{r} \cos \theta - \frac{2}{r} \cos \theta = 0$ </p>	2 1/2		
	b.	An expression for \vec{H} due to infinite length long straight conductor.			



II - IA SCHEME OF EVALUATION

Sem : 3	Subject : EMI	Sub Code : 15EC36	Date : 20-11-17
Q. No.	Bit	Description	Marks
1.	b.	<p> $\vec{r}_{12} = r\vec{a}_r - z\vec{a}_z$ $\vec{a}_{r12} = \frac{r\vec{a}_r - z\vec{a}_z}{\sqrt{r^2+z^2}}$ $d\vec{L} \times \vec{a}_{r12} = rdz\vec{a}_\phi$ $\begin{vmatrix} \vec{a}_r & r\vec{a}_\phi & \vec{a}_z \\ 0 & 0 & dz \\ r & 0 & -z \end{vmatrix}$ </p> <p> $\vec{H} = \int_{-R/2}^{R/2} \frac{Irdz\vec{a}_\phi}{4\pi(r^2+z^2)^{3/2}}$; $dH = \frac{Irdz\vec{a}_\phi}{4\pi(r^2+z^2)^{3/2}}$ $\vec{H} = \int_{z=0}^z \frac{Irdz\vec{a}_\phi}{4\pi(r^2+z^2)^{3/2}}$; $z = r \tan \theta$ $dz = r \sec^2 \theta$ $= \int_{-\pi/2}^{\pi/2} \frac{rI}{4\pi r} \cos \theta d\theta = \frac{2I}{4\pi r} \vec{a}_\phi = \frac{I}{2\pi r} \vec{a}_\phi \text{ w/m}$ </p>	6
2.	a.	<p>Capacitance per unit length of coaxial cable</p> <p> $\nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial V}{\partial r} \right) = 0$ $V = C_1 \ln r + C_2$ $V = \frac{-V_0}{\ln(b/a)} \ln r - \frac{V_0 \ln(b)}{\ln(a/b)}$ $\vec{E} = -\nabla V = -\frac{\partial V}{\partial r} \vec{a}_r = \frac{V_0}{r \ln(a/b)} \vec{a}_r \text{ V/m}$ $\vec{D} = \epsilon \vec{E} = \frac{-V_0 \epsilon}{r \ln(a/b)} \vec{a}_r = \frac{V_0 \epsilon}{r \ln(b/a)} \vec{a}_r \text{ C/m}^2$ $C = \frac{Q}{V} = \frac{V_0 \epsilon 2\pi l}{\ln(b/a) V_0} = \frac{2\pi \epsilon l}{\ln(b/a)} \text{ F}$ </p>	6

CO206.5

CO206.5

Coordinator

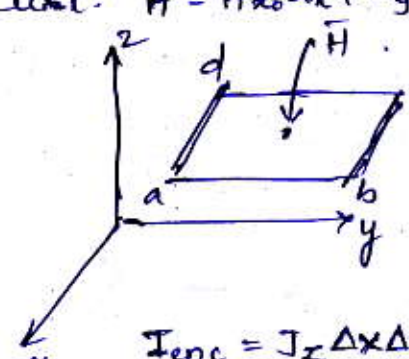
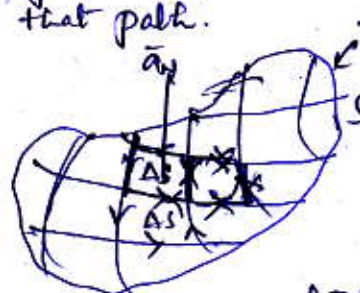
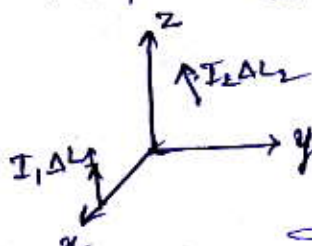
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III - IA SCHEME OF EVALUATION

Sem : 3	Subject : EMT	Sub Code : 15EC36	Date : 20/11/17
Q. No.	Bit	Description	Marks / Mapped CO's
2.	b.	<p>Curl. $\vec{H} = H_{x0}\vec{a}_x + H_{y0}\vec{a}_y + H_{z0}\vec{a}_z$</p> <p>$\vec{J} = J_x\vec{a}_x + J_y\vec{a}_y + J_z\vec{a}_z$</p>  <p>$\oint \vec{H} \cdot d\vec{l} = \Delta x \Delta y \left[\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right]$</p> <p>$\frac{\oint \vec{H} \cdot d\vec{l}}{\Delta S_z} = \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y}$</p> <p>$I_{enc} = J_z \Delta x \Delta y$</p> <p>$\lim_{\Delta y \Delta z \rightarrow 0} \frac{\oint \vec{H} \cdot d\vec{l}}{\Delta y \Delta z} = J_x = \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z}$; $\lim_{\Delta x \Delta z \rightarrow 0} \frac{\oint \vec{H} \cdot d\vec{l}}{\Delta x \Delta z} = \left[\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} \right] = J_y$</p> <p>$\text{Curl } \vec{H} = \nabla \times \vec{H} = \vec{J} \dots$</p> <p><u>Stoke's theorem:</u> "The line integral of a vector around a closed path L is equal to the integral of curl of \vec{A} over the open surface S enclosed by that path."</p>  <p>Total Surface $\cdot (\nabla \times \vec{H})_N = \frac{\oint \vec{H} \cdot d\vec{l}_{AS}}{\Delta S}$</p> <p>$(\nabla \times \vec{H})_N = (\nabla \times \vec{H}) \cdot \vec{a}_N$</p> <p>$\oint \vec{H} \cdot d\vec{l}_{AS} = (\nabla \times \vec{H}) \cdot \vec{a}_N \Delta S$</p> <p>$\oint \vec{H} \cdot d\vec{l} = \int_S (\nabla \times \vec{H}) \cdot \vec{a}_N dS$</p>	6 CO206.5
3.	a.	<p>$I_1 \vec{\Delta L}_1 = 10^5 \vec{a}_z$, $I_2 \vec{\Delta L}_2 = 10^5 (0.6 \vec{a}_x - 2 \vec{a}_y + 3 \vec{a}_z)$</p>  <p>$\vec{F}_2 = I_2 \vec{\Delta L}_2 \times d\vec{B}_1$</p> <p>$= 10^5 (0.6 \vec{a}_x - 2 \vec{a}_y + 3 \vec{a}_z) \times d\vec{B}_1$</p> <p>$= (0.5 \vec{a}_x - 1.5 \vec{a}_z) 10^{18} \text{ N}$</p> <p>$d\vec{B}_1 = \mu_0 d\vec{H}_1 = \frac{\mu_0 I_1 \vec{\Delta L}_1 \times \vec{a}_{r12}}{4\pi (r_{12})^2}$</p> <p>$= \frac{4\pi \times 10^{-7} (10^5 \vec{a}_z) \times (-\vec{a}_x)}{4\pi 2^2} = \frac{-10^5}{16\pi} \vec{a}_y \text{ A/m}$</p>	6 CO205.5



III - IA SCHEME OF EVALUATION

Sem : 3	Subject : EMT	Sub Code : 15E36	Date : 20/11/17	Marks	Mapped CO's	
3.	b.	$\nabla \times \vec{H} = \vec{J}$ $\nabla \cdot (\nabla \times \vec{H}) = \nabla \cdot \vec{J}$ $0 = \nabla \cdot \vec{J}$ but $\nabla \cdot \vec{J} = -\frac{\partial \rho_v}{\partial t}$ $\nabla \times \vec{H} = \vec{J}_c + \frac{\partial \vec{D}}{\partial t}$ $\vec{J}_c = \sigma \vec{E}$, $i_c/A = c \frac{dV}{dx} = \frac{\partial \vec{D}}{\partial t}$	$\nabla \times \vec{H} = \vec{J} + \vec{N}$ $\nabla \cdot (\nabla \times \vec{H}) = \nabla \cdot \vec{J} + \nabla \cdot \vec{N}$ $\Rightarrow \nabla \cdot \vec{N} = \nabla \cdot \frac{\partial \vec{D}}{\partial t}$ $\vec{N} = \frac{\partial \vec{D}}{\partial t}$	6+1	CO206.6	
4	a.	Derivation of boundary conditions 	$\oint \vec{B} \cdot d\vec{s} = 0$ $\Rightarrow B_{N1} = B_{N2}$ tangential: $\oint \vec{H} \cdot d\vec{l} = \int \vec{K} \cdot d\vec{w} = H_{tan1} a w - H_{tan2} a w$ $\oint \vec{H} \cdot d\vec{l} = \oint \vec{a}_{N12} \times \vec{K} = (H_{tan1} - H_{tan2})$	6	CO206.5	
	b.	Brief explanation of Maxwell's eqns. differential form Integral form	$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$ $\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$ $\nabla \cdot \vec{D} = \rho_v$ $\nabla \cdot \vec{B} = 0$	$\oint \vec{E} \cdot d\vec{l} = -\int \frac{\partial \vec{B} \cdot d\vec{s}}{\partial t}$ $\oint \vec{H} \cdot d\vec{l} = I + \int \frac{\partial \vec{D} \cdot d\vec{s}}{\partial t}$ $\oint \vec{D} \cdot d\vec{s} = \int \rho_v dV$ $\oint \vec{B} \cdot d\vec{s} = 0$	7	CO206.6