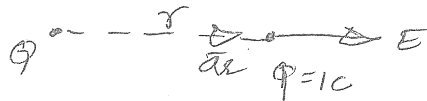


Fourth Semester BE Degree Exam - Dec 2015 / Jan. 2016

Sub: Field Theory Sub. code: 10ES36 M.Marks: 100

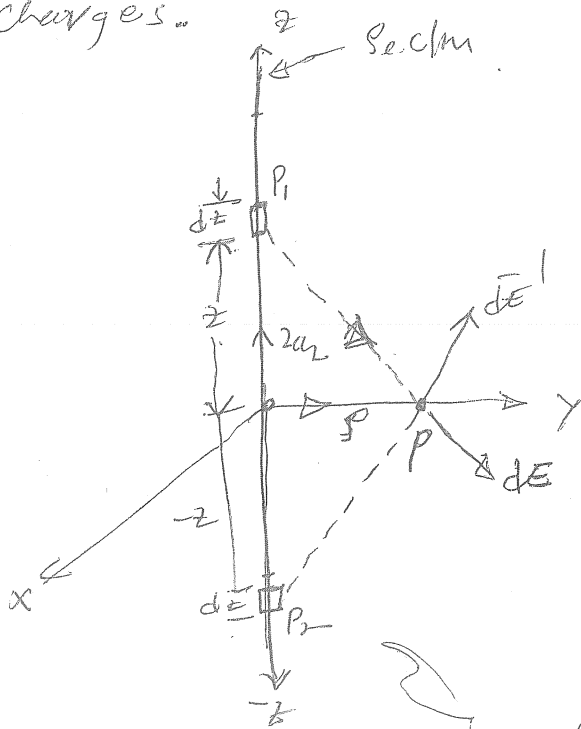
Q.1a. Explain the terms "electric field intensity" & derive expression for the field due to infinite line of charge. (08)

Soln - Electric field intensity at a point is defined as the force experienced by a unit positive charge placed at that point. It is denoted by \vec{E} & its unit is V/m or N/C . N/C or Newton/Coulomb .



$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \vec{a}_r$$

\vec{a}_r is the unit vector along the line joining the two point charges.



Consider an infinite line charge with charge density of ρ_c C/m lies along z-axis. Let us find the electric field at point P at a distance of r m from the point line conduct.

- Or.. Consider an elemental length of dz m at a distance of z m from the origin. The charge at P_1 is $dq = \rho_c \cdot dz$ (1)

The electric field at P due to an elemental charge at P_1 is given by.

$$d\vec{E} = \frac{dq}{4\pi\epsilon_0 (r_{1P})^2} \vec{a}_{r1P} \rightarrow (2)$$

From the above fig,

$$2 \vec{a}_2 + \vec{P}_1 P = 3 \vec{a}_3$$

$$\vec{P}_1 P = 3 \vec{a}_3 - 2 \vec{a}_2$$

$$|\vec{P}_1 P| = \sqrt{3^2 + 2^2} \rightarrow 3$$

$$\vec{a}_{pp} = \frac{3 \vec{a}_3 - 2 \vec{a}_2}{\sqrt{3^2 + 2^2}} \rightarrow 4$$

Putting 1, 3 & 4 in (2)

$$d\vec{E} = \frac{\rho \cdot dz}{4\pi\epsilon_0 (\sqrt{3^2 + z^2})^2} \times \frac{3 \vec{a}_3 - 2 \vec{a}_2}{\sqrt{3^2 + z^2}}$$

$$d\vec{E} = \frac{\rho \cdot dz}{4\pi\epsilon_0 (3^2 + z^2)^{3/2}} (3 \vec{a}_3 - 2 \vec{a}_2) \rightarrow (5)$$

By symmetry, the electric field at P_2 due to elemental charge at P_1 is

$$d\vec{E}' = \frac{\rho \cdot dz}{4\pi\epsilon_0 (3^2 + z^2)^{3/2}} (3 \vec{a}_3 + 2 \vec{a}_2) \rightarrow (6)$$

From eqn. 5 & 6 it is clear that z -component of electric field is equal in magnitude & opposite in direction. & hence it cancels & the y -component of electric field will add up.

$$\therefore d\vec{E} = \frac{\rho \cdot dz}{4\pi\epsilon_0 (3^2 + z^2)^{3/2}} \cdot 3 \vec{a}_3$$

$$\therefore \vec{E} = \int_{-\infty}^{+\infty} d\vec{E}$$

$$= \int_{-\infty}^{+\infty} \frac{\rho \cdot dz}{4\pi\epsilon_0 (3^2 + z^2)^{3/2}} \cdot 3 \vec{a}_3$$

put: $z = 3 \tan \theta$, $dz = 3 \sec^2 \theta d\theta$, $z = -\infty$, $\theta = \theta_1 = \tan^{-1}(-\infty) = -\pi/2$

$$\vec{E} = \rho \cdot$$

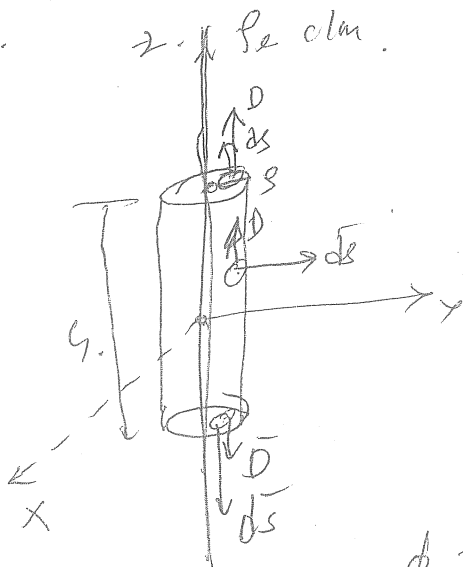
$$z = +\infty, \theta = \theta_2 = \tan^{-1}(\infty) = \pi/2$$

$$\begin{aligned}
 \therefore \vec{E} &= \frac{\rho_e \cdot \rho \cdot a_s}{4\pi\epsilon} \int_{-\pi/2}^{\pi/2} \frac{\rho \sec^2 \theta d\theta}{(\rho^2 + \rho^2 \tan^2 \theta)^{3/2}} \\
 &= \frac{\rho_e \cdot \rho^2 \cdot a_s}{4\pi\epsilon \cdot \rho^3} \int_{-\pi/2}^{\pi/2} \frac{\sec^2 \theta d\theta}{(\sec^2 \theta)^{3/2}} \\
 &= \frac{\rho_e \cdot \rho^2}{4\pi\epsilon \cdot \rho} \int_{-\pi/2}^{\pi/2} \cos \theta d\theta \\
 &= \frac{\rho_e}{4\pi\epsilon} (-\sin \theta) \Big|_{-\pi/2}^{\pi/2} \\
 &= \frac{\rho_e}{4\pi\epsilon} (\sin(\pi/2) - \sin(-\pi/2)) \\
 &= \frac{\rho_e}{4\pi\epsilon} a_x \cdot 2
 \end{aligned}$$

$$\vec{E} = \frac{\rho_e}{2\pi\epsilon} a_x \text{ N/C.}$$

6. Use Gauss law to determine electric field intensity due to infinite line charge (6)

Soln.



Consider an infinite conductor with charge density ρ_e C/m. Let us find the $E_{||}$ due to it at a r distance from the wire. Consider a closed Gaussian cylinder of radius ρ and height l . Apply Gauss law

$$\oint \vec{D} \cdot d\vec{s} = Q_{en.}$$

$$\oint_{T.S} \vec{D} \cdot d\vec{s} + \int_{B.S} \vec{D} \cdot d\vec{s} + \int_{O.S} \vec{D} \cdot d\vec{s} = Q_{en.} \rightarrow (1)$$

From the above fig $\oint_{BS} \vec{D} \cdot \vec{ds} = \oint_{BS} \vec{D} \cdot \vec{ds} = 0.$

$$\therefore \oint_{BS} \vec{D} \cdot \vec{ds} = q_{en.}$$

$$\oint_{BS} D_s \vec{a}_s \cdot \rho d\phi dz \vec{a}_z = \rho \cdot h,$$

$$\rho \int_0^{2\pi} \int_0^h D_s d\phi dz = \rho \cdot h,$$

$$\rho D_s \int_0^{2\pi} \int_0^h dz = \rho \cdot h,$$

$$\rho D_s (2\pi) (h) = \rho \cdot h.$$

$$D_s = \frac{\rho}{2\pi}$$

$$\vec{D} = D_s \vec{a}_s$$

$$\boxed{\vec{D} = \frac{\rho}{2\pi} \vec{a}_s \text{ C/m}^2}$$

$$\vec{E} = \frac{\vec{D}}{\epsilon}$$

$$\boxed{\vec{E} = \frac{\rho}{2\pi\epsilon} \vec{a}_s \text{ V/m}}$$

Q.1.C The flux density $\vec{D} = \frac{r}{3} \vec{a}_r$ nC/m² in free space.

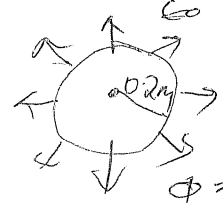
i) Find \vec{E} at $r = 0.2$ m.

ii) Find the total electric flux leaving the sphere at $r = 0.2$ m.

iii) Find the total charge within the sphere of $r = 0.3$ m.

Soln Given $\vec{D} = \frac{r}{3} \vec{a}_r$ nC/m² = $\frac{r}{3} \times 10^{-9} \vec{a}_r$ C/m², $\epsilon = \epsilon_0$

i) $\vec{E} = \frac{\vec{D}}{\epsilon_0} = \frac{r \times 10^{-9} \vec{a}_r}{3 \times 60} = \frac{0.2 \times 10^{-9} \vec{a}_r}{3 \times 60} = 7.529 \vec{a}_r$ V/m.

ii)  $\phi = \oint_{BS} \vec{D} \cdot \vec{ds} = \oint_{BS} D_r \vec{a}_r \cdot r^2 \sin\theta d\theta d\phi \vec{a}_r$
 $\phi = \oint_{BS} \frac{r}{3} \times 10^{-9} \vec{a}_r \cdot r^2 \sin\theta d\theta d\phi \vec{a}_r.$

$$\begin{aligned} \phi &= \int_S \frac{r^3 \times 10^{-9}}{3} \cdot \sin\theta \, d\theta \, d\phi \\ r &= 0.2 \, \text{m} \\ &= \frac{(0.2)^3 \times 10^{-9}}{3} \int_0^\pi \sin\theta \, d\theta \int_0^{2\pi} d\phi \\ &= 2.6667 \times 10^{-12} \left(-\cos\theta \right)_0^\pi (2\pi) \\ &= 2.6667 \times 10^{-12} \times (2) \times (2\pi) \\ \phi &= 33.51 \times 10^{-12} \text{ Coulombs} \end{aligned}$$

iii) $Q = ?$ at $r = 0.3 \, \text{m}$.

$$Q = \phi = \oint_S \vec{D} \cdot \vec{a}_n$$

$$= \oint_S \frac{r^3 \times 10^{-9}}{3} \vec{a}_r \cdot r^2 \sin\theta \, d\theta \, d\phi \, \vec{a}_r$$

$r = 0.3 \, \text{m}$

$$= \frac{r^3 \times 10^{-9}}{3} \int_S \sin\theta \, d\theta \, d\phi$$

$r = 0.3$

$$= \frac{(0.3)^3 \times 10^{-9}}{3} \int_0^\pi \sin\theta \, d\theta \int_0^{2\pi} d\phi$$

$$= 9 \times 10^{-12} \left(-\cos\theta \right)_0^\pi (2\pi)$$

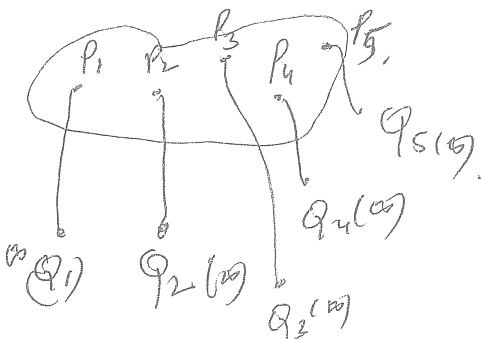
$$Q = 9 \times 10^{-12} (2) (2\pi)$$

$$Q = 113.097 \, \mu\text{C}$$

Q.2a. Show that the energy required to assemble n number of point charges is $W_E = \frac{1}{2} \sum_{m=1}^n Q_m V_m$.

Soln. & hence derive expressions for energy in electric field in terms of field quantities \vec{D} & \vec{E} .

Soln.



Consider a region shown in the fig. which is free of charge. When the point charge Q_1 is moved from outside

Eqn. 3 can be written in differential form as (4)

$$W_E = \frac{1}{2} \int_V \rho_p dV \quad (\because \rho = \rho_p dV)$$

$$W_E = \frac{1}{2} \int_V \rho_v dV \quad (\because \rho = \rho_v dV) \rightarrow (4)$$

$$W_E = \frac{1}{2} \int_S \rho_s dS \quad (\because \rho = \rho_s dS)$$

WKT. From 4

$$W_E = \frac{1}{2} \int_V (\rho_v dV) \quad (\because \rho_v = \nabla \cdot \bar{D})$$

$$= \frac{1}{2} \int_V (\nabla \cdot \bar{D}) dV \rightarrow (5)$$

For a scalar potential ϕ , & vector \bar{D} , WKT,

$$\nabla \cdot \nabla \phi = \nabla \cdot \bar{D} = \nabla \cdot \nabla \phi = \nabla^2 \phi = \rho_v$$

$$(\nabla \cdot \bar{A}) \cdot \bar{V} = \nabla \cdot \bar{V} \bar{A} - \bar{A} \cdot \nabla \bar{V}$$

$$\therefore (\nabla \cdot \bar{D}) \phi = \nabla \cdot \phi \bar{D} - \bar{D} \cdot \nabla \phi \rightarrow (6)$$

Putting (6) in (5)

$$W_E = \frac{1}{2} \int_V (\nabla \cdot \phi \bar{D} - \bar{D} \cdot \nabla \phi) dV$$

$$= \frac{1}{2} \int_V (\nabla \cdot \phi \bar{D}) dV - \frac{1}{2} \int_V \bar{D} \cdot (-\bar{E}) dV \quad (\because \bar{E} = -\nabla \phi)$$

By Divergence theorem $\int_V \nabla \cdot \bar{D} \phi dV = \oint_S \bar{D} \cdot \bar{E} \phi dS$

$$W_E = \frac{1}{2} \oint_S \phi (\bar{D} \cdot \bar{E}) dS + \frac{1}{2} \int_V \bar{D} \cdot \bar{E} dV$$

WKT, $\phi \propto \frac{1}{r}$, $d\phi \propto \frac{1}{r^2}$
 As the surface becomes ∞ , $\nabla \phi \propto \frac{1}{r^2} \propto 0$ $\therefore \oint_S \bar{D} \cdot \bar{E} \phi dS \propto \frac{1}{r} \propto 0$
 $\therefore W_E = \frac{1}{2} \int_V \bar{D} \cdot \bar{E} dV$

$$\therefore W_E = \frac{1}{2} \int_V (\bar{D} \cdot \bar{E}) dV$$

$$= \frac{1}{2} \epsilon \cdot \int_V |\bar{E}|^2 dV$$

$$(\because \bar{D} = \epsilon \bar{E})$$

$$W_E = \frac{1}{2\epsilon} \int_V (\bar{D})^2 dV$$

Hence the proof.

Q.2b. Potential is given by $V = 2(x+1)^2(y+2)^2(z+3)^2$ volts in 3D space. At a point $P(2, -1, 4)$ calculate i) potential ii) electric field intensity iii) flux density iv) volume charge density.

Solu. Given: $V = 2(x+1)^2(y+2)^2(z+3)^2$ volts, $\epsilon = \epsilon_0$, $P(2, -1, 4)$

i) $V = ?$

$$V = 2(1+2)^2(-1+2)^2(4+3)^2 = 882 \text{ volts}$$

ii) $\vec{E} = -\nabla V$

$$= - \left\{ \frac{\partial V}{\partial x} \vec{a}_x + \frac{\partial V}{\partial y} \vec{a}_y + \frac{\partial V}{\partial z} \vec{a}_z \right\}$$

$$= - \left\{ \frac{\partial}{\partial x} (2(x+1)^2(y+2)^2(z+3)^2) \vec{a}_x + \frac{\partial}{\partial y} (2(x+1)^2(y+2)^2(z+3)^2) \vec{a}_y + \frac{\partial}{\partial z} (2(x+1)^2(y+2)^2(z+3)^2) \vec{a}_z \right\}$$

$$\vec{E} = 2(y+2)^2(z+3)^2 \times 2(x+1) \vec{a}_x + (4(x+1)^2(y+2)(z+3)^2) \vec{a}_y + 4(x+1)^2(y+2)^2(z+3) \vec{a}_z$$

$$\vec{E} = 2(-2+1)^2(4+3)^2 \times 2(2+1) \vec{a}_x + 4(3)^2(1)(7)^2 \vec{a}_y + 4 \cdot 3^2 \cdot 1 \cdot 7 \vec{a}_z$$

$$\boxed{\vec{E} = 392 \vec{a}_x + 1764 \vec{a}_y + 252 \vec{a}_z \text{ N/C.}}$$

$$\vec{D} = \epsilon \vec{E}$$

iii) $\vec{D} = \epsilon_0 (392 \vec{a}_x + 1764 \vec{a}_y + 252 \vec{a}_z) \text{ C/m}^2$

iv) $\rho_{vol} = \nabla \cdot \vec{D}$

$$= \nabla \cdot \epsilon \vec{E}$$

$$= \epsilon_0 \cdot \nabla \cdot \vec{E}$$

$$= \epsilon_0 \left(\frac{\partial E_x}{\partial x} + \frac{\partial E_y}{\partial y} + \frac{\partial E_z}{\partial z} \right)$$

$$= \epsilon_0 \left(\frac{\partial}{\partial x} (4(x+1)(y+2)^2(z+3)^2) + \frac{\partial}{\partial y} (4(x+1)^2(y+2)(z+3)^2) + \frac{\partial}{\partial z} (4(x+1)^2(y+2)^2(z+3)) \right)$$

$$\rho_{vol} = \epsilon_0 (4(1)^2(7)^2 + 4 \cdot 2^2 \cdot 1 \cdot 7^2 + 4 \cdot 2^2 \cdot 1 \cdot 7)$$

$$\rho_{vol} = \epsilon_0 (1092)$$

$$\boxed{\rho_{vol} = 0.669 \times 10^{-9} \text{ C/m}^3}$$

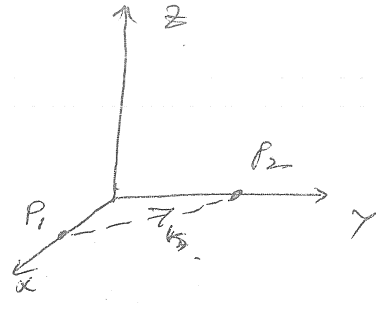
2.0. Find the work done in moving a charge of $+2C$ from $(2, 0, 0)$ to $(0, 2, 0)$ along the straight line path joining two points, if the electric field is $\vec{E} = 12x\vec{a}_x - 4y\vec{a}_y$ N/m.

Soln Given. $Q = 2C$, $\vec{E} = 12x\vec{a}_x - 4y\vec{a}_y$ N/m.
 $P_1 = (2, 0, 0)$ $P_2 = (0, 2, 0)$
 $W = ?$

$$W = -Q \int \vec{E} \cdot d\vec{l}$$

$$= -2 \int (12x\vec{a}_x - 4y\vec{a}_y) \cdot (dx\vec{a}_x + dy\vec{a}_y + dz\vec{a}_z)$$

$$W = -2 \int (12x dx - 4y dy) \rightarrow (1)$$



Equation of the straight line joining the points P_1 & P_2 is

$$\frac{x-x_1}{x_2-x_1} = \frac{y-y_1}{y_2-y_1} = \frac{z-z_1}{z_2-z_1}$$

Considering the first two terms

$$\frac{x-2}{0-2} = \frac{y-0}{2-0}$$

$$\frac{x-2}{-2} = \frac{y}{2} \Rightarrow \begin{aligned} x-2 &= -y \\ x &= 2-y \\ dx &= -dy \end{aligned}$$

\therefore Equation (1) becomes

$$W = -2 \int_0^2 12(2-y)(-dy) - 4y dy$$

$$= -2 \int_0^2 (-24 + 12y - 4y) dy$$

$$= -2 \int_0^2 (8y - 24) dy$$

$$= -2 \left(8 \frac{y^2}{2} - 24y \right)_0^2$$

$$= -2 (4(4-0) - 24(2-0))$$

$$= -2 (16 - 48)$$

$$W = 64 \text{ Joules}$$

Q.3a. Arrive at the Poisson's equation in Cartesian coordinates. Deduce Laplace's equation from Poisson's equation.

Soln. From Gauss law in point form

$$\nabla \cdot \vec{D} = \rho_v$$

$$\nabla \cdot (\epsilon \vec{E}) = \rho_v \quad (\vec{D} = \epsilon \vec{E})$$

$$\nabla \cdot \vec{E} = \frac{\rho_v}{\epsilon}$$

$$\nabla \cdot (-\nabla V) = \frac{\rho_v}{\epsilon} \quad (\vec{E} = -\nabla V)$$

$$\nabla^2 V = -\frac{\rho_v}{\epsilon} \rightarrow \text{Poisson's equation.}$$

where $\nabla^2 V$ is Laplacian operator.

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}$$

$$\nabla^2 V = \nabla \cdot \nabla V$$

$$= \nabla \cdot \left(\frac{\partial V}{\partial x} \vec{a}_x + \frac{\partial V}{\partial y} \vec{a}_y + \frac{\partial V}{\partial z} \vec{a}_z \right)$$

$$= \left(\frac{\partial}{\partial x} \vec{a}_x + \frac{\partial}{\partial y} \vec{a}_y + \frac{\partial}{\partial z} \vec{a}_z \right) \cdot \left(\frac{\partial V}{\partial x} \vec{a}_x + \frac{\partial V}{\partial y} \vec{a}_y + \frac{\partial V}{\partial z} \vec{a}_z \right)$$

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} //$$

If the region is free of charge, then $\rho_v = 0$.

$$\therefore \nabla^2 V = 0 \rightarrow \text{Laplace equation.}$$

3.6. Verify the potential field $V = 2x^2 - 3y^2 + z^2$ satisfies Laplace equation.

Soln. Given: $V = 2x^2 + 3y^2 + z^2$.

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}$$

$$= \frac{\partial^2}{\partial x^2} (2x^2 - 3y^2 + z^2) + \frac{\partial^2}{\partial y^2} (2x^2 - 3y^2 + z^2) + \frac{\partial^2}{\partial z^2} (2x^2 - 3y^2 + z^2)$$

$$\nabla^2 V = \frac{\partial}{\partial x} (4x - 0 + 0) + \frac{\partial}{\partial y} (0 - 6y + 0) + \frac{\partial}{\partial z} (0 + 0 + 2z)$$

$$= 4 - 6 + 2 = 0 // \text{ satisfies the Laplace equation.}$$

Q. 36 Using Laplace equation, derive an expression for capacitance of a Co-axial cable. 6.

Sol. Consider a coaxial cable of
 inner radius a and outer radius b .
 Let the length of the cable is L m. The Laplace equation is



$$\nabla^2 u = \frac{1}{r} \frac{\partial}{\partial r} \left(r \cdot \frac{\partial u}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 u}{\partial \phi^2} + \frac{\partial^2 u}{\partial z^2} \rightarrow (1)$$

As the potential field varies only in r -direction

$$\therefore \frac{\partial u}{\partial \phi} = \frac{\partial u}{\partial z} = 0 \quad \therefore \text{Equation (1) becomes}$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \cdot \frac{\partial u}{\partial r} \right) = 0$$

$$\frac{\partial}{\partial r} \left(r \frac{\partial u}{\partial r} \right) = 0$$

Integrating the above expression w.r.t r .

$$\int \frac{\partial}{\partial r} \left(r \cdot \frac{\partial u}{\partial r} \right) dr = 0$$

$$r \cdot \frac{\partial u}{\partial r} = C_1$$

$$\frac{\partial u}{\partial r} = \frac{C_1}{r}$$

Again integrating

$$\boxed{u = C_1 \cdot \ln r + C_2} \rightarrow (2)$$

$$u = V_0 \text{ at } r = a \quad V_0 = C_1 \cdot \ln a + C_2 \rightarrow (3)$$

$$u = 0 \text{ at } r = b \quad 0 = C_1 \cdot \ln b + C_2$$

$$V_0 = C_1 (\ln a - \ln b)$$

$$C_1 = \frac{V_0}{\ln(a/b)}$$

Putting C_1 in (3)

$$V_0 = \frac{V_0}{\ln(a/b)} \ln a + C_2$$

$$C_2 = V_0 - \frac{V_0 \cdot \ln a}{\ln(a/b)}$$

$$= \frac{V_0 (\ln a - \ln b - \ln a)}{\ln(a/b)}$$

$$C_2 = -V_0 \ln(b) / \ln(a/b)$$

$$C_2 = -V_0 \cdot \ln(b) / \ln(a/b)$$

∴ equation (1) becomes

$$V = \frac{V_0 \cdot \ln r}{\ln(a/b)} - \frac{V_0 \ln(b)}{\ln(a/b)} \quad \text{--- (3)}$$

$$\bar{E} = -\nabla V$$

$$= -\frac{\partial V}{\partial r} \bar{a}_r$$

$$= -\frac{\partial}{\partial r} \left(\frac{V_0 \cdot \ln r}{\ln(a/b)} - \frac{V_0 \ln(b)}{\ln(a/b)} \right) \bar{a}_r$$

$$\bar{E} = \left(-\frac{V_0}{r \ln(a/b)} - 0 \right) \bar{a}_r$$

$$\bar{E} = -\frac{V_0}{r \ln(a/b)} \bar{a}_r = \frac{V_0}{r \ln(b/a)} \bar{a}_r$$

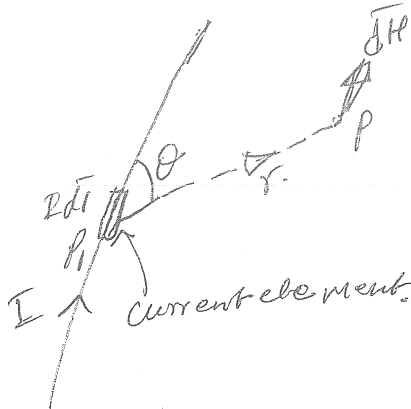
$$D = \epsilon \bar{E} = \epsilon \frac{V_0}{r \ln(b/a)} \bar{a}_r$$

$$Q = \oint_S \cdot A = \frac{\epsilon V_0}{r \ln(b/a)} \times 2\pi r \cdot L$$

$$C = \frac{Q}{V_0} = \frac{2\pi \epsilon L}{\ln(b/a)} \quad \text{Farad}$$

Q.4a. State & explain Biot-Savart law. Using this, find the magnetic field intensity in the vicinity of long straight filamentary current I Amperes along z -axis. (7)

Solu.



The magnetic field intensity at a point 'P' due to current element;

dH proportional to the product of current I & differential length ' dl ' $dH \propto I dl$
 b) the sine of the angle between the element & the line joining point P to the element, $dH \propto \sin \theta$

c) inversely proportional to the square of the distance between the point P & the current element. $dH \propto \frac{1}{r^2}$

$$\therefore dH \propto \frac{I dl \sin \theta}{r^2}$$

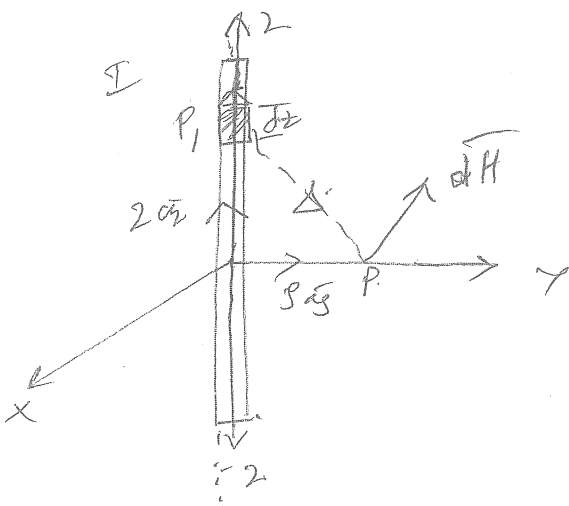
$$dH = \frac{k I dl \sin \theta}{r^2}$$

$$dH = \frac{I dl \sin \theta}{4\pi r^2} \quad (k = \frac{1}{4\pi})$$

The direction of magnetic field is normal to the plane containing the differential element Idl & the line joining the element & the point 'P'

$$\therefore \boxed{dH = \frac{I d\vec{l} \times \vec{a}_r}{4\pi r^2}} \quad \text{Atm}$$

$$\therefore \vec{H} = \int \frac{I d\vec{l} \times \vec{a}_r}{4\pi r^2}$$



Consider an infinite conductor carrying a current of I Amperes along z -axis. We wish to find the \vec{H} at a r distance from the conductor. Consider a current element $I d\vec{l}$ at P_1 . The magnetic field intensity at P due to current element at P_1 is

$$\vec{dH} = \frac{\mathbb{I} d\vec{l} \times \vec{a}_r}{4\pi r^2}$$

$$\vec{dH} = \frac{\mathbb{I} d\vec{l} \times \vec{a}_{PIP}}{4\pi (\overline{PIP})^2}$$

$$\overline{PIP} = r \vec{a}_r - 2\vec{a}_z$$

$$|\overline{PIP}| = \sqrt{r^2 + 2^2}$$

$$\vec{a}_{PIP} = \overline{PIP} / |\overline{PIP}| = \frac{r \vec{a}_r - 2\vec{a}_z}{\sqrt{r^2 + 2^2}}, \quad \mathbb{I} d\vec{l} = \mathbb{I} dz \vec{a}_z$$

$$\vec{dH} = \frac{\mathbb{I} dz \vec{a}_z \times (r \vec{a}_r - 2\vec{a}_z)}{4\pi (\sqrt{r^2 + 2^2})^2 \cdot \sqrt{r^2 + 2^2}}$$

$$\vec{dH} = \frac{\mathbb{I} dz (r \vec{a}_\phi - 0)}{4\pi (r^2 + 2^2)^{3/2}}$$

$$\vec{dH} = \frac{\mathbb{I} r dz}{4\pi (r^2 + 2^2)^{3/2}} \vec{a}_\phi$$

$$\vec{H} = \int_{-\infty}^{\infty} \frac{\mathbb{I} r dz}{4\pi (r^2 + 2^2)^{3/2}} \vec{a}_\phi$$

put $z = r \tan \theta$, $dz = r \sec^2 \theta d\theta$,

$z = -\infty$, $\theta = \theta_1 = -\pi/2$ & $z = +\infty$, $\theta = \theta_2 = \pi/2$.

$$\therefore \vec{H} = \int_{-\pi/2}^{\pi/2} \frac{\mathbb{I} r \cdot \sec^2 \theta d\theta}{4\pi (r^2 + r^2 \tan^2 \theta)^{3/2}} \vec{a}_\phi$$

$$= \frac{\mathbb{I}}{4\pi} \vec{a}_\phi \int_{-\pi/2}^{\pi/2} \frac{r^2 \sec^2 \theta d\theta}{r^3 \sec^3 \theta}$$

$$= \frac{\mathbb{I}}{4\pi r} \vec{a}_\phi \int_{-\pi/2}^{\pi/2} \cos \theta d\theta$$

$$= \frac{\mathbb{I}}{4\pi r} \vec{a}_\phi (\sin \theta) \Big|_{-\pi/2}^{\pi/2}$$

$$= \frac{\mathbb{I}}{4\pi r} \vec{a}_\phi (\sin(\pi/2) - \sin(-\pi/2))$$

$$= \frac{\mathbb{I}}{2\pi r} \vec{a}_\phi (1+1)$$

$$\boxed{\vec{H} = \frac{\mathbb{I}}{2\pi r} \vec{a}_\phi} \quad \text{Hence the proof}$$

$$\begin{aligned} \|(r^2 + r^2 \tan^2 \theta)^{3/2} &= r^3 (1 + \tan^2 \theta)^{3/2} \\ &= r^3 (\sec^2 \theta)^{3/2} \\ &= \underline{\underline{r^3 \sec^3 \theta}} \end{aligned}$$

Q.4.b. Discuss the concept of vector magnetic potential & hence show that, $\vec{A} = \frac{\mu_0}{4\pi} \int \frac{\vec{J}}{r} d\tau$ where \vec{A} is the vector magnetic potential & \vec{J} is the current density.

Soln. Vector magnetic potential is a quantity, which satisfies the following equations.

$$\vec{B} = \nabla \times \vec{A} \quad \text{--- (1)}$$

$$\nabla \cdot \vec{A} = 0 \quad \text{where } \vec{B} = \mu \vec{H}$$

WKT, from Biot-Savart law,

$$\vec{dH} = \frac{d\vec{I} \times \vec{a}_r}{4\pi r^2}$$

$$= \frac{\vec{J} \cdot d\vec{s} \cdot \vec{a}_r \times \vec{a}_r}{4\pi r^2}$$

$$(\because d\vec{I} = d\vec{s} \cdot \vec{J} = \vec{J} \cdot d\vec{s})$$

$$= \frac{\vec{J} d\tau \times \vec{a}_r}{4\pi r^2}$$

$$(\because d\vec{s} \cdot \vec{a}_r = d\tau)$$

$$\vec{dH} = \frac{\vec{J} \times \vec{a}_r d\tau}{4\pi r^2}$$

$$\vec{H} = \oint \frac{\vec{J} \times \vec{a}_r d\tau}{4\pi r^2}$$

$$= \oint \frac{\vec{J} \times \frac{\vec{a}_r}{r^2} d\tau}{4\pi}$$

$$= \oint \frac{\vec{J} \times (-\nabla(\frac{1}{r})) d\tau}{4\pi} \quad (\because \frac{\partial r}{\partial y} = -\nabla(\frac{1}{r}))$$

$$= - \int \frac{\vec{J} \times \nabla(\frac{1}{r}) d\tau}{4\pi} \quad \text{--- (2)}$$

WKT from vector identity,

$$\vec{A} \times \nabla \phi = -\nabla \times (\phi \vec{A}) + \phi (\nabla \times \vec{A})$$

$$\vec{J} \times \nabla(\frac{1}{r}) = -\nabla \times (\frac{1}{r} \vec{J}) + \frac{1}{r} (\nabla \times \vec{J})$$

For constant current density $\nabla \times \vec{J} = 0$

$$\therefore \vec{J} \times \nabla(\frac{1}{r}) = -\nabla \times \frac{\vec{J}}{r} \quad \text{--- (3)}$$

Putting (3) in (2).

$$\vec{H} = \oint \frac{\nabla \times (\frac{\vec{J}}{r}) d\tau}{4\pi}$$

$$= \nabla \times \oint \frac{\vec{J}}{r} d\tau$$

$$\text{Also, } \vec{B} = \rho \vec{H}$$

$$= \rho \nabla \times \frac{\mu}{4\pi} \int_V \frac{\vec{J}}{r} d\tau \rightarrow (4)$$

Comparing (4) & (1)

$$\vec{A} = \frac{\mu \rho}{4\pi} \int_V \frac{\vec{J}}{r} d\tau.$$

Q.4.c. At point $P(x, y, z)$, the components of vector magnetic potential are given as $A_x = 4x + 3y + 2z$, $A_y = 5x + 6y + 3z$, $A_z = 2x + 3y + 5z$. Determine \vec{B} at point P & state its nature.

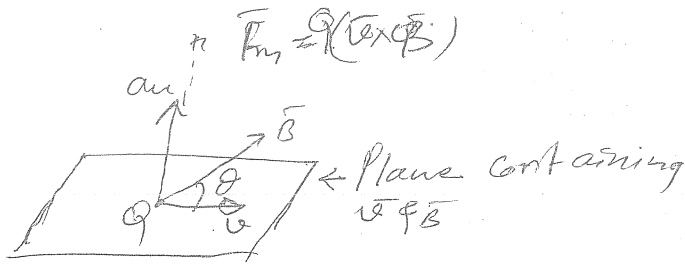
Soln.

PART-B

(9)

Q.5a. State & explain Lorentz force equation.

Soln



Consider a free charge of \$Q\$ coulombs placed in the presence of electric field

intensity. The force exerted on a charge of \$Q\$ coulombs is given by

$$\vec{F} = Q \vec{E} \longrightarrow \text{①}$$

The direction of the force is same as the direction of electric field.

Now if a moving charge is placed in a magnetic field of flux density, \$\vec{B}\$, it experiences a force. This force is a function of charge \$Q\$, velocity \$v\$, & the angle \$\theta\$ b/w \$\vec{v}\$ & \$\vec{B}\$.

The direction of this force is \$\perp\$ to the \$\vec{v}\$ & \$\vec{B}\$ & the angle \$\theta\$ w.r.t \$\vec{v}\$ & \$\vec{B}\$, i.e. \$F = qvB \sin \theta = Q \cdot \vec{v} \times \vec{B} \sin \theta\$.

Now, the total force on a moving charge due to electric field \$\vec{E}\$ & magnetic flux density \$\vec{B}\$ is

$$\boxed{\vec{F} = Q(\vec{E} + \vec{v} \times \vec{B})}$$

The above equation is known as Lorentz force equation.

5b. A conductor of 4m long lies along the \$y\$ axis with a current of 10A in the \$+y\$ direction. Find the force on the conductor if the field in the region is \$\vec{B} = 0.005 \hat{a}_x\$ Tesla.

Soln

\$l = 4\text{m}\$, \$I = 10\text{A}\$, \$\vec{B} = 0.005 \hat{a}_x\$ Tesla

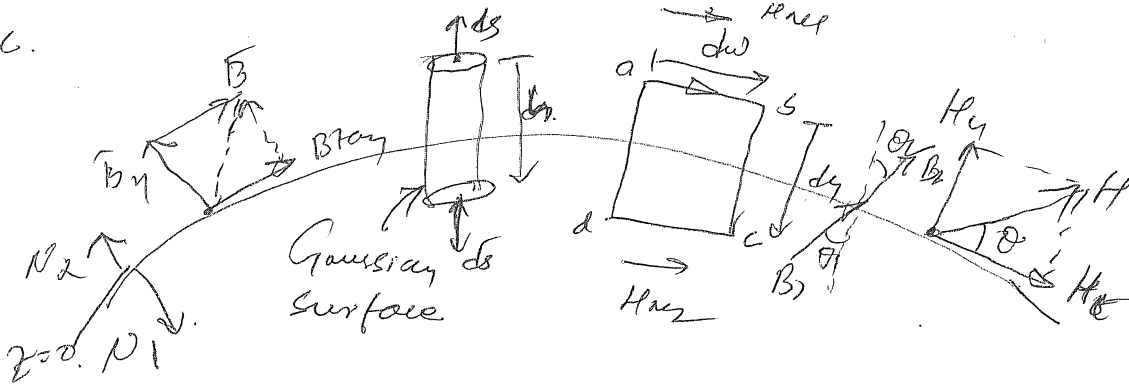
\$d\vec{F} = I d\vec{l} \times \vec{B}\$

\$\vec{F} = \int I d\vec{l} \times \vec{B}\$

\$= \int_0^4 10 dy \hat{a}_y \times 0.005 \hat{a}_x\$

\$\vec{F} = -10 \times 0.005 \int_0^4 dy \hat{a}_z = -0.05 \hat{a}_z (4) = \underline{\underline{-0.2 \hat{a}_z \text{ Newton}}}\$

Q.56.



Consider a boundary between the two magnetic medium, μ_1 & μ_2 with different magnetic permeability as shown above.

1. Boundary conditions for tangential components.

The magnetic field ^{intensity} at the interface $z=0$ in the two medium is resolved in to two components i.e. horizontal & vertical components to the interface.

Considering closed path abcd as shown above, using Ampere's law

$$\oint \vec{H} \cdot d\vec{l} = I_{enc}$$

$$\oint_{ab} \vec{H} \cdot d\vec{l} + \int_{bc} \vec{H} \cdot d\vec{l} + \int_{cd} \vec{H} \cdot d\vec{l} + \int_{da} \vec{H} \cdot d\vec{l} = I \quad \rightarrow (1)$$

At the interface $z \rightarrow 0 \therefore \int_{bc} \vec{H} \cdot d\vec{l} = \int_{cd} \vec{H} \cdot d\vec{l} = 0$

$$\int_{ab} H_{tan1} dw + (-H_{tan2}) dw = K dw$$

where K is the sheet current of K Amperes normal to the path.

$$\therefore H_{tan1} = H_{tan2}$$

$$(H_{tan1} - H_{tan2}) dl = K dl$$

$$H_{tan1} - H_{tan2} = K \quad \rightarrow (2)$$

If the surface is free from sheet current, $K=0$

$$\therefore H_{tan1} - H_{tan2} = 0$$

$$\boxed{H_{tan1} = H_{tan2}} \quad \rightarrow (3)$$

2. Boundary conditions for normal components.

Consider a closed Gaussian cylinder, as shown above, Applying Gauss law,

$$\oint_S \vec{B} \cdot d\vec{s} = 0$$

$$\oint_{TS} \vec{B} \cdot d\vec{s} + \oint_{BS} \vec{B} \cdot d\vec{s} + \oint_{CS} \vec{B} \cdot d\vec{s} = 0$$

The flux density at the interface is resolved in to horizontal & vertical components to the interface.

$$\oint_{CS} \vec{B} \cdot d\vec{s} = 0.$$

$$\oint_{TS} \vec{B} \cdot d\vec{s} + 0 + \oint_{BS} \vec{B} \cdot d\vec{s} = 0.$$

$$B_{n2} \cdot d\vec{s} + (-B_{n1}) \cdot d\vec{s} = 0$$

$$(B_{n2} - B_{n1}) \cdot d\vec{s} = 0$$

$$B_{n2} - B_{n1} = 0$$

$$\boxed{B_{n2} = B_{n1}} //$$

Q-6.9 Show that $\nabla \cdot \vec{J} = -\frac{\partial \rho_v}{\partial t}$, where \vec{J} is conduction current density, $\rho_v \Rightarrow$ volume charge

Soln From Ampere's circuital law

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

Taking divergence on both sides

$$\nabla \cdot (\nabla \times \vec{H}) = \nabla \cdot \vec{J} + \nabla \cdot \frac{\partial \vec{D}}{\partial t}$$

From vector identity $\nabla \cdot (\nabla \times \vec{H}) = 0$.

$$\therefore \nabla \cdot \vec{J} + \nabla \cdot \frac{\partial \vec{D}}{\partial t} = 0$$

$$\nabla \cdot \vec{J} = -\nabla \cdot \frac{\partial \vec{D}}{\partial t}$$

$$\nabla \cdot \vec{J} = -\frac{\partial}{\partial t} (\nabla \cdot \vec{D})$$

$$\boxed{\nabla \cdot \vec{J} = -\frac{2\mu_0}{2t}} \quad \text{Hence the proof.}$$

Q.66 $\vec{B} = 0.04 \hat{a}_y$ $v = 2.5 \sin 10^3 t$ in m/s, $B = 0$.

Assuming the conductor of length l is placed along x -axis

$$\begin{aligned} \therefore e_1 &= \int_L (\vec{v} \times \vec{B}) \cdot d\vec{l} \\ &= \int_L (2.5 \sin 10^3 t \hat{a}_z \times 0.04 \hat{a}_y) \cdot d\vec{l} \\ &= 2.5 \sin 10^3 t \times 0.04 \int_L (-\hat{a}_x) \cdot d\vec{l} \\ &= -2.5 \times 0.1 \sin 10^3 t \text{ V.} \end{aligned}$$

$$\boxed{e = -0.1 \sin 10^3 t \text{ volts}}$$

$$\begin{aligned} \vec{B} &= 0.04 \hat{a}_x \\ e_2 &= \int_L 2.5 \sin 10^3 t \hat{a}_z \times 0.04 \hat{a}_x \cdot d\vec{l} \\ &= 2.5 \times 0.04 \sin 10^3 t \int_L \hat{a}_y \cdot d\vec{l} \end{aligned}$$

$$\boxed{e_2 = 0} \quad \because \hat{a}_y \cdot \hat{a}_x = 0$$

Q. No 79. Maxwell's 2nd & 3rd equation are

$$\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t} \rightarrow 1$$

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \rightarrow 2$$

Taking curl to equation 1 on both sides.

$$\nabla \times \nabla \times \vec{E} = -\mu \nabla \times \frac{\partial \vec{H}}{\partial t}$$

$$\text{w.k.t, } \nabla \times \nabla \times \vec{E} = \nabla(\nabla \cdot \vec{E}) - \nabla^2 \vec{E}$$

$$\therefore \nabla(\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = -\mu \frac{\partial}{\partial t} (\nabla \times \vec{H})$$

$$\nabla(\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = -\mu \frac{\partial}{\partial t} \left(\vec{J} + \frac{\partial \vec{D}}{\partial t} \right)$$

from eqn 2

$$\nabla(\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = -\mu \frac{\partial \vec{J}}{\partial t} + \mu \frac{\partial^2 \vec{D}}{\partial t^2}$$

$$\vec{J} = \sigma \vec{E}$$

$$\vec{D} = \epsilon \vec{E}$$

$$\nabla^2 \vec{E} - \mu \sigma \frac{\partial \vec{E}}{\partial t} - \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2} = \nabla (\nabla \cdot \vec{E})$$

$$\nabla^2 \vec{E} - \mu \sigma \frac{\partial \vec{E}}{\partial t} - \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2} = \nabla \cdot \left(\frac{\rho_0}{\epsilon} \right) \quad \left(\begin{array}{l} \nabla \cdot \vec{D} = \rho_0 \\ \nabla \cdot \vec{E} = \frac{\rho_0}{\epsilon} \end{array} \right)$$

for free space conditions $\sigma=0, \rho_0=0$.

$$\nabla^2 \vec{E} - \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2} = 0$$

$$\boxed{\nabla^2 \vec{E} = \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2}}$$

Taking curl to eqn (2) on both sides

$$\begin{aligned} \nabla \times \nabla \times \vec{H} &= \nabla \times \vec{J}_0 + \nabla \times \frac{\partial \vec{D}}{\partial t} \\ \nabla (\nabla \cdot \vec{H}) - \nabla^2 \vec{H} &= \nabla \times \frac{\partial \vec{E}}{\partial t} + \epsilon \nabla \times \frac{\partial \vec{E}}{\partial t} \\ 0 - \nabla^2 \vec{H} &= \sigma (-\mu \frac{\partial \vec{H}}{\partial t}) + \epsilon \frac{\partial}{\partial t} (-\mu \frac{\partial \vec{H}}{\partial t}) \\ -\nabla^2 \vec{H} &= -\mu \sigma \frac{\partial \vec{H}}{\partial t} - \epsilon \mu \frac{\partial^2 \vec{H}}{\partial t^2} \end{aligned}$$

$$\nabla^2 \vec{H} - \mu \sigma \frac{\partial \vec{H}}{\partial t} - \mu \epsilon \frac{\partial^2 \vec{H}}{\partial t^2} = 0$$

for free space, $\sigma=0$.

$$\nabla^2 \vec{H} - \mu \epsilon \frac{\partial^2 \vec{H}}{\partial t^2} = 0$$

$$\boxed{\nabla^2 \vec{H} = \mu \epsilon \frac{\partial^2 \vec{H}}{\partial t^2}}$$

Q. 76 $\mu_r=1, \epsilon_r=50, \sigma=60 \text{ } \Omega/\text{m}, f=15.9 \text{ MHz}$,
 $\alpha = \beta = \nu = \eta = ?$

$$\frac{\sigma}{\omega \epsilon} = \frac{\sigma}{2\pi f \epsilon_r \epsilon_0} = \frac{60 \times 60}{2\pi \times 15.9 \times 10^6 \times 50 \times \epsilon_0}$$

$$\frac{\sigma}{\omega \epsilon} = 0.044$$

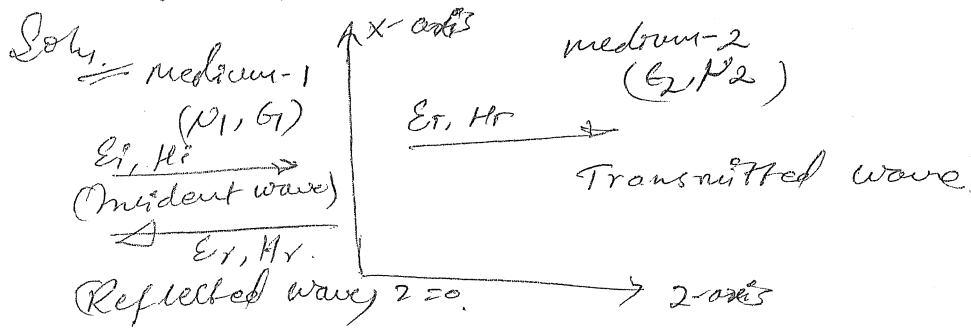
So the medium is good dielectric.

i) $\alpha = 0$ ii) $\beta = \omega \sqrt{\mu \epsilon} = 2\pi f \sqrt{\mu_0 \epsilon_0 \mu_r \epsilon_r} = 2\pi \times 15.9 \times 10^6 \sqrt{\mu_0 \epsilon_0 \times 50 \times 1} = 2.356$

iii) $\nu = \omega / \beta = \frac{2\pi \times 15.9 \times 10^6}{2.356} = 42.4 \times 10^6 \text{ m/sec}$

iv) $\eta = \sqrt{\frac{\mu_r}{\epsilon_r}} = 377 \sqrt{\frac{\mu_0}{\epsilon_0}} = 377 \sqrt{\frac{1}{50}} = 53.31 \text{ } \Omega$

Q. 8a Derive the expression for transmission coefficient & reflection coefficient.



Consider the interface at $z=0$, plane. The wave incident in medium-1. Part of the wave is transmitted in medium-2 & part of it is reflected back, as shown above. Now, in medium-1

$$\left. \begin{aligned} E_1 &= E_i + E_r \\ H_1 &= H_i + H_r \end{aligned} \right\} \rightarrow (1)$$

where, $E_i, H_i \rightarrow$ incident wave
 $E_r, H_r \rightarrow$ Reflected wave.

In medium-2.

$$\left. \begin{aligned} E_2 &= E_t \\ H_2 &= H_t \end{aligned} \right\} \rightarrow (2)$$

$H_t, E_t \rightarrow$ Transmitted electric & magnetic fields.

According to the boundary conditions,

$$E_{t \text{ on } 1} = E_{t \text{ on } 2} \quad \& \quad (H_{t \text{ on } 1} = H_{t \text{ on } 2})$$

$$\therefore E_i + E_r = E_t \rightarrow (3)$$

$$H_i + H_r = H_t \rightarrow (4)$$

$$\text{Also, } \left. \begin{aligned} E_i &= \eta_1 H_i \\ E_t &= \eta_2 H_t \\ E_r &= -\eta_1 H_r \end{aligned} \right\} \rightarrow (5)$$

Putting (5) in (3)

$$\eta_1 H_i - \eta_1 H_r = \eta_2 H_t$$

$$\frac{E_i}{\eta_1} - \frac{E_r}{\eta_1} = \frac{E_t}{\eta_2}$$

$$\text{①} - E_i - E_r = \frac{\eta_1}{\eta_2} E_t \rightarrow (6)$$

Adding equations (4) & (6)

$$2E_i = E_t \left(1 + \frac{\eta_1}{\eta_2}\right)$$

$$= E_t \frac{\eta_2 + \eta_1}{\eta_2}$$

$$\frac{E_t}{E_i} = \frac{2\eta_2}{\eta_1 + \eta_2}$$

$$\tau = \frac{E_t}{E_i} = \frac{2\eta_2}{\eta_1 + \eta_2}$$

where $\tau \rightarrow$ Transmission coefficient

putting 3 in 6

$$E_i - E_r = \frac{\eta_1}{\eta_2} (E_i + E_r)$$

$$E_i \left(1 - \frac{\eta_1}{\eta_2}\right) = E_r \left(1 + \frac{\eta_1}{\eta_2}\right)$$

$$E_i \left(\frac{\eta_2 - \eta_1}{\eta_2}\right) = E_r \left(\frac{\eta_1 + \eta_2}{\eta_2}\right)$$

$$\frac{E_r}{E_i} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$

$$\rho = \frac{E_r}{E_i} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$

where $\rho \rightarrow$ Reflection coefficient

Q.6. Write necessary expression, explain standing wave ratio.

Soln. When the reflecting wave is perfect conductor, then the entire wave is reflected back. When the reflecting medium is ^{not a} perfect conductor, then small part of the incident wave is subjected to transmission & the remaining part gets reflected back in medium. If the standing wave is setup & is given by

$$E = 2E_i \sin \alpha z \cdot \sin \beta z$$

Now there will be maximum & minimum amplitude locations. However the degree to which the field is shared between the travelling & the standing wave is identified by considering the ratio of maximum & minimum amplitudes of the wave after reflection. This ratio is known as standing wave ratio.

Consider, $\bar{E}_i = E_i e^{j(\omega t - \beta z)}$

Let, $\delta \rightarrow$ phase difference introduced due to reflection.

Then, $\bar{E}_r = E_r e^{j(\omega t + \beta z + \delta)}$

$\bar{E}_r = \Gamma E_i e^{j(\omega t + \beta z + \delta)}$ ($\because \Gamma = \frac{E_r}{E_i}$)

The resultant wave is,

$$\begin{aligned} \bar{E}_1 &= \bar{E}_i + \bar{E}_r \\ &= E_i e^{j(\omega t - \beta z)} + \Gamma E_i e^{j(\omega t + \beta z + \delta)} \\ &= E_i \left(e^{j(\omega t - \beta z)} + \Gamma e^{j(\omega t + \beta z + \delta)} \right) \end{aligned}$$

Add subtract $\Gamma e^{j(\omega t - \beta z)}$

$$\begin{aligned} \bar{E}_1 &= E_i \left[e^{j(\omega t - \beta z)} + \Gamma e^{j(\omega t + \beta z + \delta)} + \Gamma e^{j(\omega t - \beta z)} - \Gamma e^{j(\omega t - \beta z)} \right] \\ &= E_i \left[(1 + \Gamma) e^{j(\omega t - \beta z)} + \Gamma (-e^{j(\omega t + \beta z)} + e^{j(\omega t + \beta z + \delta)}) \right] \end{aligned}$$

$\delta = \pi$ for β reflection, & considering the real part of above eqn

$$\bar{E}_1 = E_i \left[(1 + \Gamma) \cos(\omega t - \beta z) + 2\Gamma \sin \omega t \sin \beta z \right]$$

The second term is called standing wave.

Now $E_{max} = E_i + E_r$, & $E_{min} = E_i - E_r$.

$$\therefore SWR = \frac{E_{max}}{E_{min}} = \frac{E_i + E_r}{E_i - E_r} = \frac{E_i + \Gamma E_i}{E_i - \Gamma E_i} = \frac{1 + \Gamma}{1 - \Gamma}$$

$$SWR = \frac{1 + \Gamma}{1 - \Gamma}$$